

TER WorkSheet: New dwelling design stage

User Details:

Assessor Name:

Stroma Number:

Software Name: Stroma FSAP 2012

Software Version:

Version: 1.0.5.41

Property Address: HONE House Anon

Address : House , 1 Main Street, CH11 XYZ

1. Overall dwelling dimensions:

| | Area(m ²) | | Av. Height(m) | | Volume(m ³) |
|---|-----------------------|--------|---------------|--------------------------------------|-------------------------|
| Ground floor | 48.58 | (1a) x | 2.75 | (2a) = | 133.6 |
| First floor | 43.22 | (1b) x | 2.65 | (2b) = | 114.53 |
| Second floor | 43.22 | (1c) x | 2.44 | (2c) = | 105.46 |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n) | 135.02 | (4) | | | |
| Dwelling volume | | | | (3a)+(3b)+(3c)+(3d)+(3e)+.....(3n) = | 353.58 |

2. Ventilation rate:

| | main heating | | secondary heating | | other | | total | | m ³ per hour |
|------------------------------|--------------|---|-------------------|---|-------|---|-------|--------|-------------------------|
| Number of chimneys | 0 | + | 0 | + | 0 | = | 0 | x 40 = | 0 |
| Number of open flues | 0 | + | 0 | + | 0 | = | 0 | x 20 = | 0 |
| Number of intermittent fans | | | | | | | 4 | x 10 = | 40 |
| Number of passive vents | | | | | | | 0 | x 10 = | 0 |
| Number of flueless gas fires | | | | | | | 0 | x 40 = | 0 |

Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 40 ÷ (5) = 0.11 (8)

If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)

Number of storeys in the dwelling (ns) 0 (9)

Additional infiltration [(9)-1]x0.1 = 0 (10)

Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction 0 (11)

if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35

If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0 0 (12)

If no draught lobby, enter 0.05, else enter 0 0 (13)

Percentage of windows and doors draught stripped 0 (14)

Window infiltration $0.25 - [0.2 \times (14) \div 100] =$ 0 (15)

Infiltration rate $(8) + (10) + (11) + (12) + (13) + (15) =$ 0 (16)

Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area 5 (17)

If based on air permeability value, then (18) = [(17) ÷ 20]+(8), otherwise (18) = (16) 0.36 (18)

Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used

Number of sides sheltered 0 (19)

Shelter factor $(20) = 1 - [0.075 \times (19)] =$ 1 (20)

Infiltration rate incorporating shelter factor $(21) = (18) \times (20) =$ 0.36 (21)

Infiltration rate modified for monthly wind speed

| | | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Monthly average wind speed from Table 7

(22)m=

| | | | | | | | | | | | |
|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|

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Wind Factor (22a)m = (22)m ÷ 4

| | | | | | | | | | | | | |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 |
|---------|------|------|------|-----|------|------|------|------|---|------|------|------|

Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

| | | | | | | | | | | | |
|------|------|------|-----|------|------|------|------|------|------|------|------|
| 0.46 | 0.45 | 0.44 | 0.4 | 0.39 | 0.34 | 0.34 | 0.34 | 0.36 | 0.39 | 0.41 | 0.43 |
|------|------|------|-----|------|------|------|------|------|------|------|------|

Calculate effective air change rate for the applicable case

If mechanical ventilation:

| | |
|---|-------|
| 0 | (23a) |
|---|-------|

If exhaust air heat pump using Appendix N, (23b) = (23a) x Fmv (equation (N5)) , otherwise (23b) = (23a)

| | |
|---|-------|
| 0 | (23b) |
|---|-------|

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

| | |
|---|-------|
| 0 | (23c) |
|---|-------|

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) x [1 - (23c) ÷ 100]

| | | | | | | | | | | | | | |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|-------|
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (24a) |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|-------|

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

| | | | | | | | | | | | | | |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|-------|
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (24b) |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|-------|

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 x (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 x (23b)

| | | | | | | | | | | | | | |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|-------|
| (24c)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (24c) |
|---------|---|---|---|---|---|---|---|---|---|---|---|---|-------|

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

| | | | | | | | | | | | | | |
|---------|------|-----|-----|------|------|------|------|------|------|------|------|------|-------|
| (24d)m= | 0.61 | 0.6 | 0.6 | 0.58 | 0.58 | 0.56 | 0.56 | 0.56 | 0.57 | 0.58 | 0.58 | 0.59 | (24d) |
|---------|------|-----|-----|------|------|------|------|------|------|------|------|------|-------|

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

| | | | | | | | | | | | | | |
|--------|------|-----|-----|------|------|------|------|------|------|------|------|------|------|
| (25)m= | 0.61 | 0.6 | 0.6 | 0.58 | 0.58 | 0.56 | 0.56 | 0.56 | 0.57 | 0.58 | 0.58 | 0.59 | (25) |
|--------|------|-----|-----|------|------|------|------|------|------|------|------|------|------|

3. Heat losses and heat loss parameter:

| ELEMENT | Gross area (m²) | Openings m² | Net Area A ,m² | U-value W/m²K | A X U (W/K) | k-value kJ/m²·K | A X k kJ/K |
|-----------------|-----------------|-------------|----------------|--------------------|-------------|-----------------|------------|
| Doors | | | 3.74 | x 1.2 | = 4.488 | | (26) |
| Windows Type 1 | | | 1.27 | x 1/[1/(1.4)+0.04] | = 1.68 | | (27) |
| Windows Type 2 | | | 1.27 | x 1/[1/(1.4)+0.04] | = 1.68 | | (27) |
| Windows Type 3 | | | 1.27 | x 1/[1/(1.4)+0.04] | = 1.68 | | (27) |
| Windows Type 4 | | | 1.27 | x 1/[1/(1.4)+0.04] | = 1.68 | | (27) |
| Windows Type 5 | | | 7.64 | x 1/[1/(1.4)+0.04] | = 10.13 | | (27) |
| Windows Type 6 | | | 1.16 | x 1/[1/(1.4)+0.04] | = 1.54 | | (27) |
| Windows Type 7 | | | 1.27 | x 1/[1/(1.4)+0.04] | = 1.68 | | (27) |
| Windows Type 8 | | | 0.56 | x 1/[1/(1.4)+0.04] | = 0.74 | | (27) |
| Windows Type 9 | | | 1.36 | x 1/[1/(1.4)+0.04] | = 1.8 | | (27) |
| Windows Type 10 | | | 1.74 | x 1/[1/(1.4)+0.04] | = 2.31 | | (27) |
| Windows Type 11 | | | 0.65 | x 1/[1/(1.4)+0.04] | = 0.86 | | (27) |
| Windows Type 12 | | | 1.74 | x 1/[1/(1.4)+0.04] | = 2.31 | | (27) |
| Windows Type 13 | | | 0.56 | x 1/[1/(1.4)+0.04] | = 0.74 | | (27) |
| Windows Type 14 | | | 0.56 | x 1/[1/(1.4)+0.04] | = 0.74 | | (27) |
| Windows Type 15 | | | 1.05 | x 1/[1/(1.4)+0.04] | = 1.39 | | (27) |
| Windows Type 16 | | | 1.05 | x 1/[1/(1.4)+0.04] | = 1.39 | | (27) |

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| | | | | | | | | |
|--|--------|-------|-----------|-------------------------------|-----------|-----|--------|-------|
| Windows Type 17 | | | 1.63 | $\times 1/[1/(1.4) + 0.04] =$ | 2.16 | | | (27) |
| Windows Type 18 | | | 0.65 | $\times 1/[1/(1.4) + 0.04] =$ | 0.86 | | | (27) |
| Windows Type 19 | | | 1.63 | $\times 1/[1/(1.4) + 0.04] =$ | 2.16 | | | (27) |
| Windows Type 20 | | | 0.56 | $\times 1/[1/(1.4) + 0.04] =$ | 0.74 | | | (27) |
| Windows Type 21 | | | 0.56 | $\times 1/[1/(1.4) + 0.04] =$ | 0.74 | | | (27) |
| Rooflights | | | 0.5588519 | $\times 1/[1/(1.7) + 0.04] =$ | 0.9500483 | | | (27b) |
| Floor | | | 48.58 | \times | 0.13 | $=$ | 6.3154 | (28) |
| Walls | 200.77 | 33.19 | 167.58 | \times | 0.18 | $=$ | 30.16 | (29) |
| Roof Type1 | 16.69 | 0.56 | 16.13 | \times | 0.13 | $=$ | 2.1 | (30) |
| Roof Type2 | 26.56 | 0 | 26.56 | \times | 0.13 | $=$ | 3.45 | (30) |
| Roof Type3 | 2.62 | 0 | 2.62 | \times | 0.13 | $=$ | 0.34 | (30) |
| Total area of elements, m ² | | | 295.22 | | | | | (31) |

* for windows and roof windows, use effective window U-value calculated using formula $1/[(1/U\text{-value})+0.04]$ as given in paragraph 3.2

** include the areas on both sides of internal walls and partitions

| | | | |
|--|---------------------------------------|-------|------|
| Fabric heat loss, W/K = S (A x U) | (26)...(30) + (32) = | 86.79 | (33) |
| Heat capacity Cm = S(A x k) | ((28)...(30) + (32) + (32a)...(32e) = | 0 | (34) |
| Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m ² K | Indicative Value: Medium | 250 | (35) |

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

| | | | |
|---|--------------------|-------|------|
| Thermal bridges : S (L x Y) calculated using Appendix K | (36) = 0.05 x (31) | 16.8 | (36) |
| Total fabric heat loss | (33) + (36) = | 103.6 | (37) |

| Ventilation heat loss calculated monthly | (38)m = 0.33 x (25)m x (5) | | (38) | | | | | | | | | | | | | | | | | | | | | | | | |
|--|----------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| | | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> <tr> <td>70.85</td> <td>70.36</td> <td>69.89</td> <td>67.65</td> <td>67.23</td> <td>65.28</td> <td>65.28</td> <td>64.92</td> <td>66.03</td> <td>67.23</td> <td>68.08</td> <td>68.96</td> </tr> </table> | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | 70.85 | 70.36 | 69.89 | 67.65 | 67.23 | 65.28 | 65.28 | 64.92 | 66.03 | 67.23 | 68.08 | 68.96 | |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | | | | | | | | | | | | | | | |
| 70.85 | 70.36 | 69.89 | 67.65 | 67.23 | 65.28 | 65.28 | 64.92 | 66.03 | 67.23 | 68.08 | 68.96 | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | |
|--------------------------------|----------------------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| Heat transfer coefficient, W/K | (39)m = (37) + (38)m | | (39) | | | | | | | | | | | | |
| | | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>174.44</td> <td>173.96</td> <td>173.48</td> <td>171.25</td> <td>170.83</td> <td>168.88</td> <td>168.88</td> <td>168.52</td> <td>169.63</td> <td>170.83</td> <td>171.67</td> <td>172.56</td> </tr> </table> | 174.44 | 173.96 | 173.48 | 171.25 | 170.83 | 168.88 | 168.88 | 168.52 | 169.63 | 170.83 | 171.67 | 172.56 | |
| 174.44 | 173.96 | 173.48 | 171.25 | 170.83 | 168.88 | 168.88 | 168.52 | 169.63 | 170.83 | 171.67 | 172.56 | | | | |
| | | Average = Sum(39) _{1...12} / 12 = | 171.24 | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | |
|---|---------------------|--|------|------|------|------|------|------|------|------|------|------|------|------|--|
| Heat loss parameter (HLP), W/m ² K | (40)m = (39)m ÷ (4) | | (40) | | | | | | | | | | | | |
| | | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>1.29</td> <td>1.29</td> <td>1.28</td> <td>1.27</td> <td>1.27</td> <td>1.25</td> <td>1.25</td> <td>1.25</td> <td>1.26</td> <td>1.27</td> <td>1.27</td> <td>1.28</td> </tr> </table> | 1.29 | 1.29 | 1.28 | 1.27 | 1.27 | 1.25 | 1.25 | 1.25 | 1.26 | 1.27 | 1.27 | 1.28 | |
| 1.29 | 1.29 | 1.28 | 1.27 | 1.27 | 1.25 | 1.25 | 1.25 | 1.26 | 1.27 | 1.27 | 1.28 | | | | |
| | | Average = Sum(40) _{1...12} / 12 = | 1.27 | | | | | | | | | | | | |

| Number of days in month (Table 1a) | | | (41) | | | | | | | | | | | | | | | | | | | | | | | | |
|------------------------------------|---|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|----|----|----|----|----|----|----|----|----|----|----|--|--|
| | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> <tr> <td>31</td> <td>28</td> <td>31</td> <td>30</td> <td>31</td> <td>30</td> <td>31</td> <td>31</td> <td>30</td> <td>31</td> <td>30</td> <td>31</td> </tr> </table> | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | | | | | | | | | | | | | | | |
| 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | | | | | | | | | | | | | | |

4. Water heating energy requirement: kWh/year:

| | | |
|---|------|------|
| Assumed occupancy, N | 2.91 | (42) |
| if TFA > 13.9, N = 1 + 1.76 x [1 - exp(-0.000349 x (TFA - 13.9) ²)] + 0.0013 x (TFA - 13.9) | | |
| if TFA ≤ 13.9, N = 1 | | |

| | | |
|--|--------|------|
| Annual average hot water usage in litres per day Vd,average = (25 x N) + 36 | 103.24 | (43) |
| Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold) | | |

| Hot water usage in litres per day for each month Vd,m = factor from Table 1c x (43) | | | (44) | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|-------------------------------------|---------|-------|-------|-------|-------|--------|-------|--------|--------|-----|-----|--------|--------|-------|--------|-------|-------|-------|-------|--------|-------|--------|--------|--|--|
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| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | | | | | | | | | | | | | | | |
| 113.56 | 109.43 | 105.3 | 101.17 | 97.05 | 92.92 | 92.92 | 97.05 | 101.17 | 105.3 | 109.43 | 113.56 | | | | | | | | | | | | | | | | |
| | | Total = Sum(44) _{1...12} = | 1238.88 | | | | | | | | | | | | | | | | | | | | | | | | |

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Energy content of hot water used - calculated monthly = $4.190 \times Vd,m \times nm \times DTm / 3600$ kWh/month (see Tables 1b, 1c, 1d)

| | | | | | | | | | | | | | |
|-------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|------|
| (45)m= | 168.41 | 147.29 | 151.99 | 132.51 | 127.15 | 109.72 | 101.67 | 116.67 | 118.06 | 137.59 | 150.19 | 163.1 | |
| Total = Sum(45) _{1...12} = | | | | | | | | | | | | 1624.36 | (45) |

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

| | | | | | | | | | | | | | |
|--------|-------|-------|------|-------|-------|-------|-------|------|-------|-------|-------|-------|--|
| (46)m= | 25.26 | 22.09 | 22.8 | 19.88 | 19.07 | 16.46 | 15.25 | 17.5 | 17.71 | 20.64 | 22.53 | 24.46 | |
|--------|-------|-------|------|-------|-------|-------|-------|------|-------|-------|-------|-------|--|

Water storage loss:

| | | |
|---|-----|------|
| Storage volume (litres) including any solar or WWHRS storage within same vessel | 150 | (47) |
|---|-----|------|

If community heating and no tank in dwelling, enter 110 litres in (47)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in (47)

Water storage loss:

| | | |
|---|------|------|
| a) If manufacturer's declared loss factor is known (kWh/day): | 2.11 | (48) |
|---|------|------|

| | | |
|----------------------------------|------|------|
| Temperature factor from Table 2b | 0.54 | (49) |
|----------------------------------|------|------|

| | | |
|---|------|------|
| Energy lost from water storage, kWh/year (48) x (49) = | 1.14 | (50) |
|---|------|------|

b) If manufacturer's declared cylinder loss factor is not known:

| | | |
|--|---|------|
| Hot water storage loss factor from Table 2 (kWh/litre/day) | 0 | (51) |
|--|---|------|

If community heating see section 4.3

| | | |
|-----------------------------|---|------|
| Volume factor from Table 2a | 0 | (52) |
|-----------------------------|---|------|

| | | |
|----------------------------------|---|------|
| Temperature factor from Table 2b | 0 | (53) |
|----------------------------------|---|------|

| | | |
|---|---|------|
| Energy lost from water storage, kWh/year (47) x (51) x (52) x (53) = | 0 | (54) |
|---|---|------|

| | | |
|----------------------------|------|------|
| Enter (50) or (54) in (55) | 1.14 | (55) |
|----------------------------|------|------|

Water storage loss calculated for each month ((56)m = (55) x (41)m

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (56)m= | 35.37 | 31.94 | 35.37 | 34.23 | 35.37 | 34.23 | 35.37 | 35.37 | 34.23 | 35.37 | 34.23 | 35.37 | (56) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) - (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (57)m= | 35.37 | 31.94 | 35.37 | 34.23 | 35.37 | 34.23 | 35.37 | 35.37 | 34.23 | 35.37 | 34.23 | 35.37 | (57) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

| | | |
|--|---|------|
| Primary circuit loss (annual) from Table 3 | 0 | (58) |
|--|---|------|

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 x (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (59)m= | 23.26 | 21.01 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 | (59) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

Combi loss calculated for each month (61)m = (60) ÷ 365 x (41)m

| | | | | | | | | | | | | | |
|--------|---|---|---|---|---|---|---|---|---|---|---|---|------|
| (61)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (61) |
|--------|---|---|---|---|---|---|---|---|---|---|---|---|------|

Total heat required for water heating calculated for each month (62)m = $0.85 \times (45)m + (46)m + (57)m + (59)m + (61)m$

| | | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|--------|--------|--------|------|
| (62)m= | 227.04 | 200.25 | 210.62 | 189.25 | 185.78 | 166.46 | 160.3 | 175.3 | 174.8 | 196.22 | 206.93 | 221.73 | (62) |
|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|--------|--------|--------|------|

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRS applies, see Appendix G)

| | | | | | | | | | | | | | |
|--------|---|---|---|---|---|---|---|---|---|---|---|---|------|
| (63)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (63) |
|--------|---|---|---|---|---|---|---|---|---|---|---|---|------|

Output from water heater

| | | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|--------|--------|--------|--|
| (64)m= | 227.04 | 200.25 | 210.62 | 189.25 | 185.78 | 166.46 | 160.3 | 175.3 | 174.8 | 196.22 | 206.93 | 221.73 | |
|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|--------|--------|--------|--|

Output from water heater (annual)_{1...12} = 2314.67 (64)

Heat gains from water heating, kWh/month $0.25 \times [0.85 \times (45)m + (61)m] + 0.8 \times [(46)m + (57)m + (59)m]$

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|--------|------|
| (65)m= | 102.9 | 91.34 | 97.44 | 89.45 | 89.18 | 81.87 | 80.71 | 85.7 | 84.65 | 92.65 | 95.33 | 101.13 | (65) |
|--------|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|--------|------|

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

| | | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|
| (66)m= | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | 145.35 | (66) |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|------|-------|------|------|-------|-------|-------|------|-------|------|
| (67)m= | 27.07 | 24.05 | 19.56 | 14.8 | 11.07 | 9.34 | 10.1 | 13.12 | 17.61 | 22.36 | 26.1 | 27.83 | (67) |
|--------|-------|-------|-------|------|-------|------|------|-------|-------|-------|------|-------|------|

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

| | | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|
| (68)m= | 303.67 | 306.83 | 298.89 | 281.98 | 260.64 | 240.58 | 227.18 | 224.03 | 231.97 | 248.88 | 270.22 | 290.28 | (68) |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (69)m= | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | 37.53 | (69) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

Pumps and fans gains (Table 5a)

| | | | | | | | | | | | | | |
|--------|---|---|---|---|---|---|---|---|---|---|---|---|------|
| (70)m= | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | (70) |
|--------|---|---|---|---|---|---|---|---|---|---|---|---|------|

Losses e.g. evaporation (negative values) (Table 5)

| | | | | | | | | | | | | | |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|------|
| (71)m= | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | -116.28 | (71) |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|------|

Water heating gains (Table 5)

| | | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|------|
| (72)m= | 138.31 | 135.92 | 130.97 | 124.24 | 119.87 | 113.71 | 108.48 | 115.18 | 117.56 | 124.53 | 132.4 | 135.93 | (72) |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|------|

Total internal gains = (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

| | | | | | | | | | | | | | |
|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|
| (73)m= | 538.66 | 536.4 | 519.01 | 490.63 | 461.18 | 433.24 | 415.36 | 421.94 | 436.75 | 465.38 | 498.33 | 523.64 | (73) |
|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

| Orientation: | Access Factor Table 6d | x | Area m ² | x | Flux Table 6a | x | g _g Table 6b | x | FF Table 6c | = | Gains (W) | | | |
|--------------|---------------------------|---|------------------------|---|------------------|---|----------------------------|---|----------------|---|--------------|---|-------|------|
| North | 0.9x | | 0.77 | x | 1.16 | x | 10.63 | x | 0.63 | x | 0.7 | = | 3.77 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 20.32 | x | 0.63 | x | 0.7 | = | 7.2 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 34.53 | x | 0.63 | x | 0.7 | = | 12.24 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 55.46 | x | 0.63 | x | 0.7 | = | 19.66 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 74.72 | x | 0.63 | x | 0.7 | = | 26.49 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 79.99 | x | 0.63 | x | 0.7 | = | 28.36 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 74.68 | x | 0.63 | x | 0.7 | = | 26.47 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 59.25 | x | 0.63 | x | 0.7 | = | 21 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 41.52 | x | 0.63 | x | 0.7 | = | 14.72 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 24.19 | x | 0.63 | x | 0.7 | = | 8.58 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 13.12 | x | 0.63 | x | 0.7 | = | 4.65 | (74) |
| North | 0.9x | | 0.77 | x | 1.16 | x | 8.86 | x | 0.63 | x | 0.7 | = | 3.14 | (74) |
| East | 0.9x | | 0.77 | x | 1.27 | x | 19.64 | x | 0.63 | x | 0.7 | = | 7.62 | (76) |
| East | 0.9x | | 0.77 | x | 1.27 | x | 19.64 | x | 0.63 | x | 0.7 | = | 7.62 | (76) |
| East | 0.9x | | 0.77 | x | 1.27 | x | 19.64 | x | 0.63 | x | 0.7 | = | 7.62 | (76) |
| East | 0.9x | | 0.77 | x | 1.27 | x | 19.64 | x | 0.63 | x | 0.7 | = | 7.62 | (76) |
| East | 0.9x | | 0.77 | x | 0.65 | x | 19.64 | x | 0.63 | x | 0.7 | = | 3.9 | (76) |
| East | 0.9x | | 0.77 | x | 1.74 | x | 19.64 | x | 0.63 | x | 0.7 | = | 10.44 | (76) |
| East | 0.9x | | 0.77 | x | 1.63 | x | 19.64 | x | 0.63 | x | 0.7 | = | 9.78 | (76) |
| East | 0.9x | | 0.77 | x | 0.65 | x | 19.64 | x | 0.63 | x | 0.7 | = | 3.9 | (76) |

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|------|------|------|---|------|---|--------|---|------|---|-----|---|-------|------|
| East | 0.9x | 0.77 | x | 1.63 | x | 19.64 | x | 0.63 | x | 0.7 | = | 9.78 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 38.42 | x | 0.63 | x | 0.7 | = | 14.91 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 38.42 | x | 0.63 | x | 0.7 | = | 14.91 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 38.42 | x | 0.63 | x | 0.7 | = | 14.91 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 38.42 | x | 0.63 | x | 0.7 | = | 14.91 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 38.42 | x | 0.63 | x | 0.7 | = | 7.63 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 38.42 | x | 0.63 | x | 0.7 | = | 20.43 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 38.42 | x | 0.63 | x | 0.7 | = | 19.14 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 38.42 | x | 0.63 | x | 0.7 | = | 7.63 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 38.42 | x | 0.63 | x | 0.7 | = | 19.14 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 63.27 | x | 0.63 | x | 0.7 | = | 24.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 63.27 | x | 0.63 | x | 0.7 | = | 24.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 63.27 | x | 0.63 | x | 0.7 | = | 24.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 63.27 | x | 0.63 | x | 0.7 | = | 24.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 63.27 | x | 0.63 | x | 0.7 | = | 24.56 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 63.27 | x | 0.63 | x | 0.7 | = | 12.57 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 63.27 | x | 0.63 | x | 0.7 | = | 33.65 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 63.27 | x | 0.63 | x | 0.7 | = | 31.52 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 63.27 | x | 0.63 | x | 0.7 | = | 12.57 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 63.27 | x | 0.63 | x | 0.7 | = | 31.52 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 92.28 | x | 0.63 | x | 0.7 | = | 35.82 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 92.28 | x | 0.63 | x | 0.7 | = | 35.82 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 92.28 | x | 0.63 | x | 0.7 | = | 35.82 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 92.28 | x | 0.63 | x | 0.7 | = | 35.82 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 92.28 | x | 0.63 | x | 0.7 | = | 35.82 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 92.28 | x | 0.63 | x | 0.7 | = | 18.33 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 92.28 | x | 0.63 | x | 0.7 | = | 49.07 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 92.28 | x | 0.63 | x | 0.7 | = | 45.97 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 92.28 | x | 0.63 | x | 0.7 | = | 18.33 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 92.28 | x | 0.63 | x | 0.7 | = | 45.97 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 113.09 | x | 0.63 | x | 0.7 | = | 43.89 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 113.09 | x | 0.63 | x | 0.7 | = | 43.89 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 113.09 | x | 0.63 | x | 0.7 | = | 43.89 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 113.09 | x | 0.63 | x | 0.7 | = | 43.89 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 113.09 | x | 0.63 | x | 0.7 | = | 43.89 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 113.09 | x | 0.63 | x | 0.7 | = | 22.47 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 113.09 | x | 0.63 | x | 0.7 | = | 60.14 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 113.09 | x | 0.63 | x | 0.7 | = | 56.34 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 113.09 | x | 0.63 | x | 0.7 | = | 22.47 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 113.09 | x | 0.63 | x | 0.7 | = | 56.34 | (76) |

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|------|------|------|---|------|---|--------|---|------|---|-----|---|-------|------|
| East | 0.9x | 0.77 | x | 1.27 | x | 115.77 | x | 0.63 | x | 0.7 | = | 44.93 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 115.77 | x | 0.63 | x | 0.7 | = | 44.93 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 115.77 | x | 0.63 | x | 0.7 | = | 44.93 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 115.77 | x | 0.63 | x | 0.7 | = | 44.93 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 115.77 | x | 0.63 | x | 0.7 | = | 44.93 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 115.77 | x | 0.63 | x | 0.7 | = | 23 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 115.77 | x | 0.63 | x | 0.7 | = | 61.56 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 115.77 | x | 0.63 | x | 0.7 | = | 57.67 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 115.77 | x | 0.63 | x | 0.7 | = | 23 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 115.77 | x | 0.63 | x | 0.7 | = | 57.67 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 110.22 | x | 0.63 | x | 0.7 | = | 42.78 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 110.22 | x | 0.63 | x | 0.7 | = | 42.78 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 110.22 | x | 0.63 | x | 0.7 | = | 42.78 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 110.22 | x | 0.63 | x | 0.7 | = | 42.78 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 110.22 | x | 0.63 | x | 0.7 | = | 21.89 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 110.22 | x | 0.63 | x | 0.7 | = | 58.61 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 110.22 | x | 0.63 | x | 0.7 | = | 54.91 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 110.22 | x | 0.63 | x | 0.7 | = | 21.89 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 110.22 | x | 0.63 | x | 0.7 | = | 54.91 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 94.68 | x | 0.63 | x | 0.7 | = | 36.75 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 94.68 | x | 0.63 | x | 0.7 | = | 36.75 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 94.68 | x | 0.63 | x | 0.7 | = | 36.75 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 94.68 | x | 0.63 | x | 0.7 | = | 36.75 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 94.68 | x | 0.63 | x | 0.7 | = | 36.75 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 94.68 | x | 0.63 | x | 0.7 | = | 18.81 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 94.68 | x | 0.63 | x | 0.7 | = | 50.35 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 94.68 | x | 0.63 | x | 0.7 | = | 47.16 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 94.68 | x | 0.63 | x | 0.7 | = | 18.81 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 94.68 | x | 0.63 | x | 0.7 | = | 47.16 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 73.59 | x | 0.63 | x | 0.7 | = | 28.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 73.59 | x | 0.63 | x | 0.7 | = | 28.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 73.59 | x | 0.63 | x | 0.7 | = | 28.56 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 73.59 | x | 0.63 | x | 0.7 | = | 28.56 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 73.59 | x | 0.63 | x | 0.7 | = | 14.62 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 73.59 | x | 0.63 | x | 0.7 | = | 39.13 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 73.59 | x | 0.63 | x | 0.7 | = | 36.66 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 73.59 | x | 0.63 | x | 0.7 | = | 14.62 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 73.59 | x | 0.63 | x | 0.7 | = | 36.66 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 45.59 | x | 0.63 | x | 0.7 | = | 17.69 | (76) |

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|-------|------|------|---|------|---|-------|---|------|---|-----|---|--------|------|
| East | 0.9x | 0.77 | x | 1.27 | x | 45.59 | x | 0.63 | x | 0.7 | = | 17.69 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 45.59 | x | 0.63 | x | 0.7 | = | 17.69 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 45.59 | x | 0.63 | x | 0.7 | = | 17.69 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 45.59 | x | 0.63 | x | 0.7 | = | 17.69 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 45.59 | x | 0.63 | x | 0.7 | = | 9.06 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 45.59 | x | 0.63 | x | 0.7 | = | 24.24 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 45.59 | x | 0.63 | x | 0.7 | = | 22.71 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 45.59 | x | 0.63 | x | 0.7 | = | 9.06 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 45.59 | x | 0.63 | x | 0.7 | = | 22.71 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 24.49 | x | 0.63 | x | 0.7 | = | 9.5 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 24.49 | x | 0.63 | x | 0.7 | = | 9.5 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 24.49 | x | 0.63 | x | 0.7 | = | 9.5 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 24.49 | x | 0.63 | x | 0.7 | = | 9.5 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 24.49 | x | 0.63 | x | 0.7 | = | 9.5 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 24.49 | x | 0.63 | x | 0.7 | = | 4.86 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 24.49 | x | 0.63 | x | 0.7 | = | 13.02 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 24.49 | x | 0.63 | x | 0.7 | = | 12.2 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 24.49 | x | 0.63 | x | 0.7 | = | 4.86 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 24.49 | x | 0.63 | x | 0.7 | = | 12.2 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 16.15 | x | 0.63 | x | 0.7 | = | 6.27 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 16.15 | x | 0.63 | x | 0.7 | = | 6.27 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 16.15 | x | 0.63 | x | 0.7 | = | 6.27 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 16.15 | x | 0.63 | x | 0.7 | = | 6.27 | (76) |
| East | 0.9x | 0.77 | x | 1.27 | x | 16.15 | x | 0.63 | x | 0.7 | = | 6.27 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 16.15 | x | 0.63 | x | 0.7 | = | 3.21 | (76) |
| East | 0.9x | 0.77 | x | 1.74 | x | 16.15 | x | 0.63 | x | 0.7 | = | 8.59 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 16.15 | x | 0.63 | x | 0.7 | = | 8.05 | (76) |
| East | 0.9x | 0.77 | x | 0.65 | x | 16.15 | x | 0.63 | x | 0.7 | = | 3.21 | (76) |
| East | 0.9x | 0.77 | x | 1.63 | x | 16.15 | x | 0.63 | x | 0.7 | = | 8.05 | (76) |
| South | 0.9x | 0.77 | x | 7.64 | x | 46.75 | x | 0.63 | x | 0.7 | = | 109.16 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 46.75 | x | 0.63 | x | 0.7 | = | 8 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 46.75 | x | 0.63 | x | 0.7 | = | 19.43 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 46.75 | x | 0.63 | x | 0.7 | = | 24.86 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 46.75 | x | 0.63 | x | 0.7 | = | 15 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 46.75 | x | 0.63 | x | 0.7 | = | 15 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 76.57 | x | 0.63 | x | 0.7 | = | 178.78 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 76.57 | x | 0.63 | x | 0.7 | = | 13.1 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 76.57 | x | 0.63 | x | 0.7 | = | 31.82 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 76.57 | x | 0.63 | x | 0.7 | = | 40.72 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 76.57 | x | 0.63 | x | 0.7 | = | 24.57 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 76.57 | x | 0.63 | x | 0.7 | = | 24.57 | (78) |

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|-------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South | 0.9x | 0.77 | x | 7.64 | x | 97.53 | x | 0.63 | x | 0.7 | = | 227.73 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 97.53 | x | 0.63 | x | 0.7 | = | 16.69 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 97.53 | x | 0.63 | x | 0.7 | = | 40.54 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 97.53 | x | 0.63 | x | 0.7 | = | 51.87 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 97.53 | x | 0.63 | x | 0.7 | = | 31.3 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 97.53 | x | 0.63 | x | 0.7 | = | 31.3 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 110.23 | x | 0.63 | x | 0.7 | = | 257.38 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 110.23 | x | 0.63 | x | 0.7 | = | 18.87 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 110.23 | x | 0.63 | x | 0.7 | = | 45.82 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 110.23 | x | 0.63 | x | 0.7 | = | 58.62 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 110.23 | x | 0.63 | x | 0.7 | = | 35.37 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 110.23 | x | 0.63 | x | 0.7 | = | 35.37 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 114.87 | x | 0.63 | x | 0.7 | = | 268.21 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 114.87 | x | 0.63 | x | 0.7 | = | 19.66 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 114.87 | x | 0.63 | x | 0.7 | = | 47.74 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 114.87 | x | 0.63 | x | 0.7 | = | 61.08 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 114.87 | x | 0.63 | x | 0.7 | = | 36.86 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 114.87 | x | 0.63 | x | 0.7 | = | 36.86 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 110.55 | x | 0.63 | x | 0.7 | = | 258.12 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 110.55 | x | 0.63 | x | 0.7 | = | 18.92 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 110.55 | x | 0.63 | x | 0.7 | = | 45.95 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 110.55 | x | 0.63 | x | 0.7 | = | 58.79 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 110.55 | x | 0.63 | x | 0.7 | = | 35.47 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 110.55 | x | 0.63 | x | 0.7 | = | 35.47 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 108.01 | x | 0.63 | x | 0.7 | = | 252.2 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 108.01 | x | 0.63 | x | 0.7 | = | 18.49 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 108.01 | x | 0.63 | x | 0.7 | = | 44.89 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 108.01 | x | 0.63 | x | 0.7 | = | 57.44 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 108.01 | x | 0.63 | x | 0.7 | = | 34.66 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 108.01 | x | 0.63 | x | 0.7 | = | 34.66 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 104.89 | x | 0.63 | x | 0.7 | = | 244.92 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 104.89 | x | 0.63 | x | 0.7 | = | 17.95 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 104.89 | x | 0.63 | x | 0.7 | = | 43.6 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 104.89 | x | 0.63 | x | 0.7 | = | 55.78 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 104.89 | x | 0.63 | x | 0.7 | = | 33.66 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 104.89 | x | 0.63 | x | 0.7 | = | 33.66 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 101.89 | x | 0.63 | x | 0.7 | = | 237.89 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 101.89 | x | 0.63 | x | 0.7 | = | 17.44 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 101.89 | x | 0.63 | x | 0.7 | = | 42.35 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 101.89 | x | 0.63 | x | 0.7 | = | 54.18 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 101.89 | x | 0.63 | x | 0.7 | = | 32.69 | (78) |

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|-------|------|------|---|------|---|--------|---|------|---|-----|---|--------|------|
| South | 0.9x | 0.77 | x | 1.05 | x | 101.89 | x | 0.63 | x | 0.7 | = | 32.69 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 82.59 | x | 0.63 | x | 0.7 | = | 192.83 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 82.59 | x | 0.63 | x | 0.7 | = | 14.13 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 82.59 | x | 0.63 | x | 0.7 | = | 34.33 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 82.59 | x | 0.63 | x | 0.7 | = | 43.92 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 82.59 | x | 0.63 | x | 0.7 | = | 26.5 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 82.59 | x | 0.63 | x | 0.7 | = | 26.5 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 55.42 | x | 0.63 | x | 0.7 | = | 129.39 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 55.42 | x | 0.63 | x | 0.7 | = | 9.48 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 55.42 | x | 0.63 | x | 0.7 | = | 23.03 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 55.42 | x | 0.63 | x | 0.7 | = | 29.47 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 55.42 | x | 0.63 | x | 0.7 | = | 17.78 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 55.42 | x | 0.63 | x | 0.7 | = | 17.78 | (78) |
| South | 0.9x | 0.77 | x | 7.64 | x | 40.4 | x | 0.63 | x | 0.7 | = | 94.32 | (78) |
| South | 0.9x | 0.77 | x | 0.56 | x | 40.4 | x | 0.63 | x | 0.7 | = | 6.91 | (78) |
| South | 0.9x | 0.77 | x | 1.36 | x | 40.4 | x | 0.63 | x | 0.7 | = | 16.79 | (78) |
| South | 0.9x | 0.77 | x | 1.74 | x | 40.4 | x | 0.63 | x | 0.7 | = | 21.48 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 40.4 | x | 0.63 | x | 0.7 | = | 12.96 | (78) |
| South | 0.9x | 0.77 | x | 1.05 | x | 40.4 | x | 0.63 | x | 0.7 | = | 12.96 | (78) |
| West | 0.9x | 0.77 | x | 0.56 | x | 19.64 | x | 0.63 | x | 0.7 | = | 3.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 19.64 | x | 0.63 | x | 0.7 | = | 3.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 19.64 | x | 0.63 | x | 0.7 | = | 3.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 19.64 | x | 0.63 | x | 0.7 | = | 3.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 38.42 | x | 0.63 | x | 0.7 | = | 6.58 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 38.42 | x | 0.63 | x | 0.7 | = | 6.58 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 38.42 | x | 0.63 | x | 0.7 | = | 6.58 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 63.27 | x | 0.63 | x | 0.7 | = | 10.83 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 63.27 | x | 0.63 | x | 0.7 | = | 10.83 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 63.27 | x | 0.63 | x | 0.7 | = | 10.83 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 63.27 | x | 0.63 | x | 0.7 | = | 10.83 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 92.28 | x | 0.63 | x | 0.7 | = | 15.79 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 92.28 | x | 0.63 | x | 0.7 | = | 15.79 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 92.28 | x | 0.63 | x | 0.7 | = | 15.79 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 92.28 | x | 0.63 | x | 0.7 | = | 15.79 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 113.09 | x | 0.63 | x | 0.7 | = | 19.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 113.09 | x | 0.63 | x | 0.7 | = | 19.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 113.09 | x | 0.63 | x | 0.7 | = | 19.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 113.09 | x | 0.63 | x | 0.7 | = | 19.36 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 115.77 | x | 0.63 | x | 0.7 | = | 19.81 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 115.77 | x | 0.63 | x | 0.7 | = | 19.81 | (80) |

TER WorkSheet: New dwelling design stage

| | | | | | | | | | | | | | |
|------------|------|------|---|------|---|--------|---|------|---|-----|---|-------|------|
| West | 0.9x | 0.77 | x | 0.56 | x | 115.77 | x | 0.63 | x | 0.7 | = | 19.81 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 115.77 | x | 0.63 | x | 0.7 | = | 19.81 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 110.22 | x | 0.63 | x | 0.7 | = | 18.86 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 110.22 | x | 0.63 | x | 0.7 | = | 18.86 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 110.22 | x | 0.63 | x | 0.7 | = | 18.86 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 94.68 | x | 0.63 | x | 0.7 | = | 16.2 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 94.68 | x | 0.63 | x | 0.7 | = | 16.2 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 94.68 | x | 0.63 | x | 0.7 | = | 16.2 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 94.68 | x | 0.63 | x | 0.7 | = | 16.2 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 73.59 | x | 0.63 | x | 0.7 | = | 12.59 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 73.59 | x | 0.63 | x | 0.7 | = | 12.59 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 73.59 | x | 0.63 | x | 0.7 | = | 12.59 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 73.59 | x | 0.63 | x | 0.7 | = | 12.59 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 45.59 | x | 0.63 | x | 0.7 | = | 7.8 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 45.59 | x | 0.63 | x | 0.7 | = | 7.8 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 45.59 | x | 0.63 | x | 0.7 | = | 7.8 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 45.59 | x | 0.63 | x | 0.7 | = | 7.8 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 24.49 | x | 0.63 | x | 0.7 | = | 4.19 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 24.49 | x | 0.63 | x | 0.7 | = | 4.19 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 24.49 | x | 0.63 | x | 0.7 | = | 4.19 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 24.49 | x | 0.63 | x | 0.7 | = | 4.19 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 16.15 | x | 0.63 | x | 0.7 | = | 2.76 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 16.15 | x | 0.63 | x | 0.7 | = | 2.76 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 16.15 | x | 0.63 | x | 0.7 | = | 2.76 | (80) |
| West | 0.9x | 0.77 | x | 0.56 | x | 16.15 | x | 0.63 | x | 0.7 | = | 2.76 | (80) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 15.3 | x | 0.63 | x | 0.7 | = | 3.39 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 28.48 | x | 0.63 | x | 0.7 | = | 6.32 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 50.24 | x | 0.63 | x | 0.7 | = | 11.14 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 89.03 | x | 0.63 | x | 0.7 | = | 19.75 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 129.88 | x | 0.63 | x | 0.7 | = | 28.81 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 143.74 | x | 0.63 | x | 0.7 | = | 31.88 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 132.31 | x | 0.63 | x | 0.7 | = | 29.35 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 98.56 | x | 0.63 | x | 0.7 | = | 21.86 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 62.62 | x | 0.63 | x | 0.7 | = | 13.89 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 34.05 | x | 0.63 | x | 0.7 | = | 7.55 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 18.64 | x | 0.63 | x | 0.7 | = | 4.14 | (82) |
| Rooflights | 0.9x | 1 | x | 0.56 | x | 12.94 | x | 0.63 | x | 0.7 | = | 2.87 | (82) |

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=

| | | | | | | | | | | | |
|-----|--------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| 288 | 501.92 | 710.74 | 910.77 | 1040.36 | 1039.78 | 999.71 | 903.26 | 780.73 | 561.79 | 347.17 | 244.95 |
|-----|--------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|

 (83)

Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=

| | | | | | | | | | | | |
|--------|---------|---------|--------|---------|---------|---------|--------|---------|---------|-------|--------|
| 826.65 | 1038.32 | 1229.75 | 1401.4 | 1501.53 | 1473.02 | 1415.07 | 1325.2 | 1217.48 | 1027.17 | 845.5 | 768.59 |
|--------|---------|---------|--------|---------|---------|---------|--------|---------|---------|-------|--------|

 (84)

TER WorkSheet: New dwelling design stage

7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C) 21 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
|--------|-----|------|------|------|------|------|------|------|------|------|------|-----|------|
| (86)m= | 1 | 0.99 | 0.98 | 0.94 | 0.85 | 0.68 | 0.51 | 0.56 | 0.81 | 0.97 | 0.99 | 1 | (86) |

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

| | | | | | | | | | | | | | |
|--------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (87)m= | 19.58 | 19.8 | 20.11 | 20.49 | 20.78 | 20.94 | 20.99 | 20.98 | 20.87 | 20.47 | 19.95 | 19.55 | (87) |
|--------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (88)m= | 19.85 | 19.85 | 19.85 | 19.87 | 19.87 | 19.88 | 19.88 | 19.88 | 19.88 | 19.87 | 19.86 | 19.86 | (88) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

| | | | | | | | | | | | | | |
|--------|---|------|------|------|------|------|------|------|------|------|------|---|------|
| (89)m= | 1 | 0.99 | 0.97 | 0.92 | 0.79 | 0.58 | 0.39 | 0.44 | 0.72 | 0.95 | 0.99 | 1 | (89) |
|--------|---|------|------|------|------|------|------|------|------|------|------|---|------|

Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (90)m= | 17.97 | 18.29 | 18.74 | 19.28 | 19.66 | 19.84 | 19.88 | 19.87 | 19.78 | 19.26 | 18.52 | 17.93 | (90) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

fLA = Living area ÷ (4) = 0.15 (91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (92)m= | 18.22 | 18.52 | 18.95 | 19.46 | 19.83 | 20.01 | 20.05 | 20.04 | 19.94 | 19.44 | 18.73 | 18.18 | (92) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

Apply adjustment to the mean internal temperature from Table 4e, where appropriate

| | | | | | | | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| (93)m= | 18.22 | 18.52 | 18.95 | 19.46 | 19.83 | 20.01 | 20.05 | 20.04 | 19.94 | 19.44 | 18.73 | 18.18 | (93) |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|

8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

Utilisation factor for gains, hm:

| | | | | | | | | | | | | | |
|--------|---|------|------|------|------|------|------|------|------|------|------|---|------|
| (94)m= | 1 | 0.99 | 0.97 | 0.91 | 0.79 | 0.59 | 0.41 | 0.46 | 0.73 | 0.94 | 0.99 | 1 | (94) |
|--------|---|------|------|------|------|------|------|------|------|------|------|---|------|

Useful gains, hmGm , W = (94)m x (84)m

| | | | | | | | | | | | | | |
|--------|--------|---------|---------|---------|---------|--------|--------|--------|--------|--------|-------|--------|------|
| (95)m= | 822.74 | 1024.99 | 1188.35 | 1275.21 | 1186.06 | 874.61 | 576.52 | 605.06 | 889.34 | 965.78 | 836.4 | 765.93 | (95) |
|--------|--------|---------|---------|---------|---------|--------|--------|--------|--------|--------|-------|--------|------|

Monthly average external temperature from Table 8

| | | | | | | | | | | | | | |
|--------|-----|-----|-----|-----|------|------|------|------|------|------|-----|-----|------|
| (96)m= | 4.3 | 4.9 | 6.5 | 8.9 | 11.7 | 14.6 | 16.6 | 16.4 | 14.1 | 10.6 | 7.1 | 4.2 | (96) |
|--------|-----|-----|-----|-----|------|------|------|------|------|------|-----|-----|------|

Heat loss rate for mean internal temperature, Lm , W =[(39)m x [(93)m– (96)m]

| | | | | | | | | | | | | | |
|--------|---------|---------|---------|---------|---------|--------|-------|--------|--------|---------|---------|---------|------|
| (97)m= | 2427.89 | 2369.06 | 2159.69 | 1808.77 | 1389.35 | 913.99 | 581.8 | 613.97 | 991.42 | 1510.87 | 1997.28 | 2412.11 | (97) |
|--------|---------|---------|---------|---------|---------|--------|-------|--------|--------|---------|---------|---------|------|

Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

| | | | | | | | | | | | | | |
|---|---------|--------|--------|--------|--------|---|---|---|---|--------|--------|---------|------|
| (98)m= | 1194.23 | 903.21 | 722.67 | 384.16 | 151.25 | 0 | 0 | 0 | 0 | 405.54 | 835.83 | 1224.76 | |
| Total per year (kWh/year) = Sum(98) _{1...5,9...12} = | | | | | | | | | | | | 5821.66 | (98) |

Space heating requirement in kWh/m²/year 43.12 (99)

9a. Energy requirements – Individual heating systems including micro-CHP

Space heating:

Fraction of space heat from secondary/supplementary system 0 (201)

Fraction of space heat from main system(s) (202) = 1 – (201) = 1 (202)

Fraction of total heating from main system 1 (204) = (202) × [1 – (203)] = 1 (204)

Efficiency of main space heating system 1 93.5 (206)

Efficiency of secondary/supplementary heating system, % 0 (208)

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| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | kWh/year |
|---|--------|--------|--------|--------|-----|-----|-----|-----|--------|--------|---------|----------|
| Space heating requirement (calculated above) | | | | | | | | | | | | |
| 1194.23 | 903.21 | 722.67 | 384.16 | 151.25 | 0 | 0 | 0 | 0 | 405.54 | 835.83 | 1224.76 | |
| $(211)m = \{[(98)m \times (204)]\} \times 100 \div (206)$ | | | | | | | | | | | | (211) |
| 1277.25 | 966 | 772.91 | 410.87 | 161.76 | 0 | 0 | 0 | 0 | 433.74 | 893.94 | 1309.9 | |
| $Total (kWh/year) = Sum(211)_{1..5,10..12} =$ | | | | | | | | | | | 6226.37 | (211) |
| Space heating fuel (secondary), kWh/month | | | | | | | | | | | | |
| $= \{[(98)m \times (201)]\} \times 100 \div (208)$ | | | | | | | | | | | | |
| $(215)m =$ | | | | | | | | | | | | |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| $Total (kWh/year) = Sum(215)_{1..5,10..12} =$ | | | | | | | | | | | 0 | (215) |

Water heating

| | | | | | | | | | | | | | |
|---|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|-------|-------|
| Output from water heater (calculated above) | | | | | | | | | | | | | |
| 227.04 | 200.25 | 210.62 | 189.25 | 185.78 | 166.46 | 160.3 | 175.3 | 174.8 | 196.22 | 206.93 | 221.73 | | |
| Efficiency of water heater | | | | | | | | | | | | 79.8 | (216) |
| $(217)m =$ | | | | | | | | | | | | | |
| 88.6 | 88.35 | 87.84 | 86.66 | 84.27 | 79.8 | 79.8 | 79.8 | 79.8 | 86.71 | 88.15 | 88.68 | | |
| Fuel for water heating, kWh/month | | | | | | | | | | | | | |
| $(219)m = (64)m \times 100 \div (217)m$ | | | | | | | | | | | | | |
| $(219)m =$ | | | | | | | | | | | | | |
| 256.25 | 226.65 | 239.78 | 218.37 | 220.45 | 208.59 | 200.88 | 219.67 | 219.05 | 226.3 | 234.73 | 250.04 | | |
| $Total = Sum(219a)_{1..12} =$ | | | | | | | | | | | 2720.76 | (219) | |

Annual totals

| | | | |
|--|----------------------------------|---------|--------|
| Space heating fuel used, main system 1 | kWh/year | 6226.37 | |
| Water heating fuel used | kWh/year | 2720.76 | |
| Electricity for pumps, fans and electric keep-hot central heating pump: | 30 | | (230c) |
| boiler with a fan-assisted flue | 45 | | (230e) |
| Total electricity for the above, kWh/year | $sum\ of\ (230a) \dots (230g) =$ | 75 | (231) |
| Electricity for lighting | | 478.11 | (232) |
| Total delivered energy for all uses (211)...(221) + (231) + (232)...(237b) = | | 9500.24 | (338) |

12a. CO2 emissions – Individual heating systems including micro-CHP

| | Energy kWh/year | Emission factor kg CO2/kWh | Emissions kg CO2/year |
|---|---------------------------------|-------------------------------|--------------------------|
| Space heating (main system 1) | (211) x | 0.216 | = 1344.9 (261) |
| Space heating (secondary) | (215) x | 0.519 | = 0 (263) |
| Water heating | (219) x | 0.216 | = 587.68 (264) |
| Space and water heating | (261) + (262) + (263) + (264) = | | 1932.58 (265) |
| Electricity for pumps, fans and electric keep-hot | (231) x | 0.519 | = 38.93 (267) |
| Electricity for lighting | (232) x | 0.519 | = 248.14 (268) |
| Total CO2, kg/year | $sum\ of\ (265) \dots (271) =$ | | 2219.65 (272) |

TER = 24.31 (273)

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